Analysis and development of polymer electrolyte membrane fuel cell power generation systems

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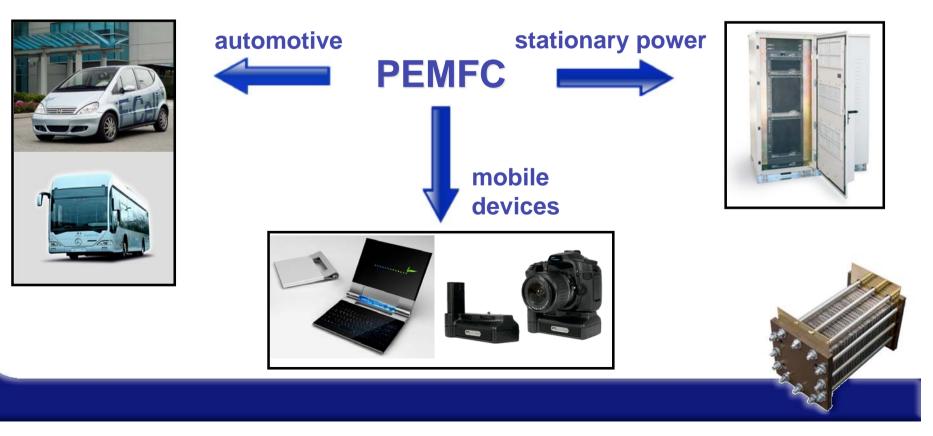
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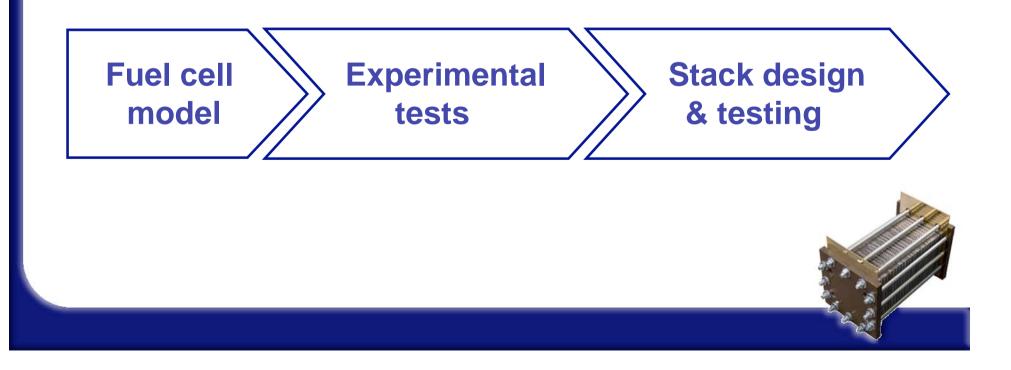
Motivation and objectives

Power generation systems based on **fuel cells** represent a **promising technology** for the future. The main reasons are related to the **efficiency** of the energy conversion which is higher than that of other technologies and to the **lower emissions** level.



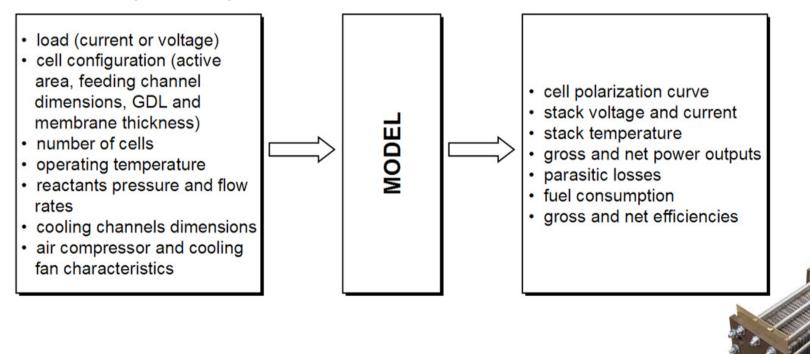
Motivation and objectives

This study aims to identify, through experiments and simulations, the main aspects concerning the PEMFC systems operation and to put into practice the acquired know-how during the design and development phase of a PEMFC stack.



Fuel cell stack model

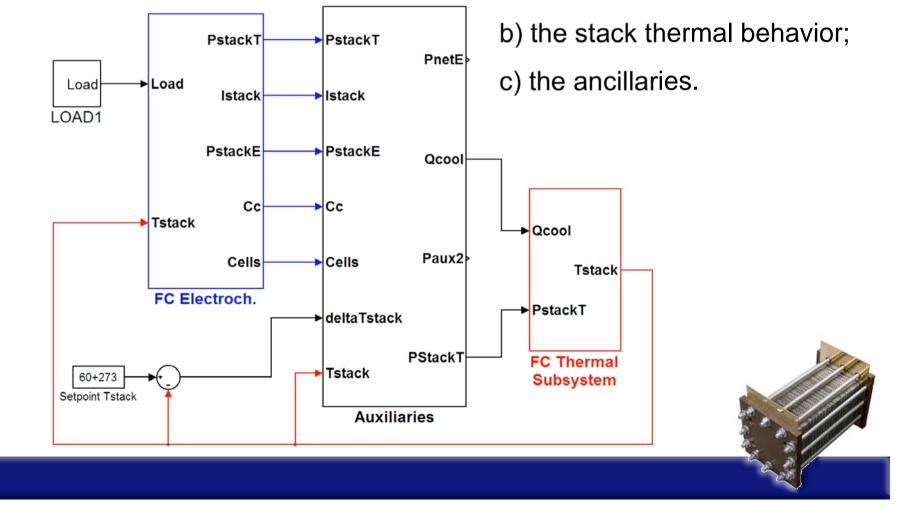
The present work proposes a model which integrates the finite element method in a dynamic simulation, in order to achieve a higher accuracy and the possibility to investigate the influence of various parameters on the fuel cell system dynamics.



Fuel cell stack model

The model is implemented using Matlab/Simulink and consists of three

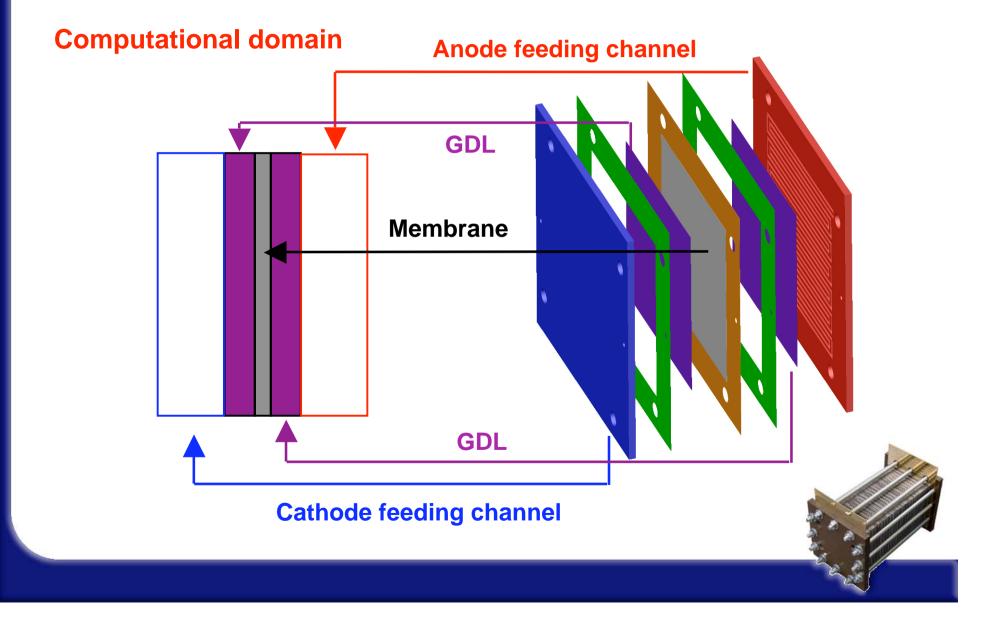
interacting main subsystems that simulate: a) the stack electrochemistry;



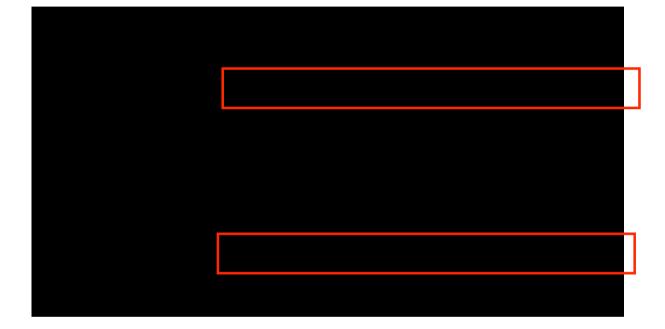
The electrochemical model was realized in **Femlab**, the mass transport and electrochemical phenomena being simulated with the differential equations implemented in various *application modes*.

Assumptions

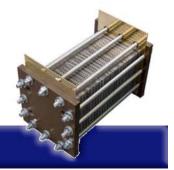
- ✓ ideal gas mixtures;
- \checkmark isothermal;
- ✓ incompressible and laminar flow;
- ✓ homogeneous electrodes;
- ✓ impermeable membrane;
- \checkmark zero-thickness active layers.



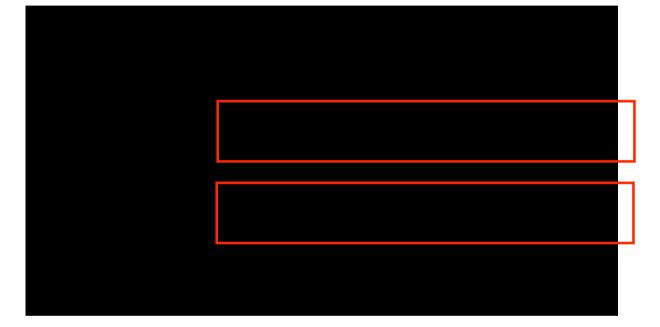
Equations



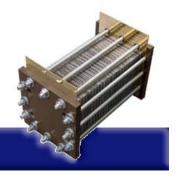
$$\eta \nabla^2 \mathbf{u} = \frac{\nabla p}{\rho} + \mathbf{u} \cdot \nabla \mathbf{u}$$
 Navier Stokes Eq

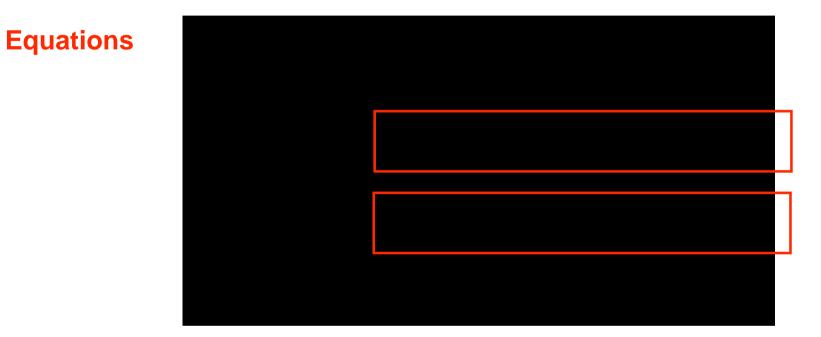


Equations



$$-\nabla p = \mathbf{u} \cdot \frac{\eta}{k} - \eta \nabla^2 \mathbf{u}$$
 Brinkman Eq.

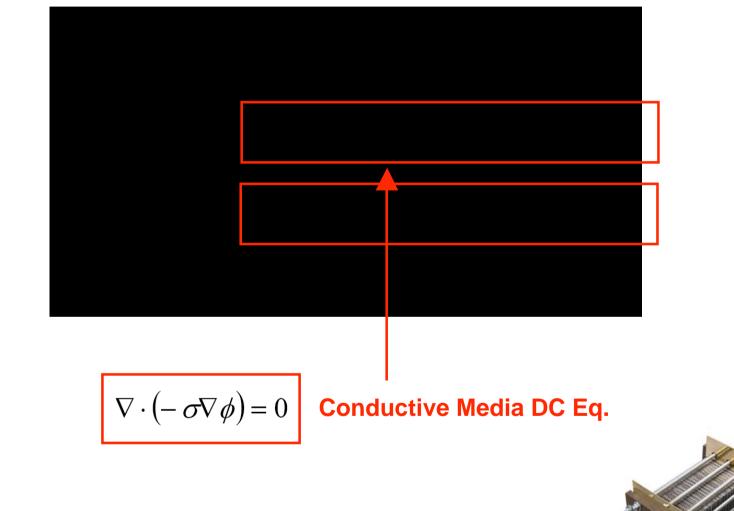




$$\nabla \cdot \left[-\rho w_i \sum_j D_{ij}^{eff} \left\{ \frac{M}{M_j} \left(\nabla w_j + w_j \frac{\nabla M}{M} \right) + \left(x_j - w_j \right) \frac{\nabla p}{p} \right\} + w_i \rho \mathbf{u} \right] = 0$$

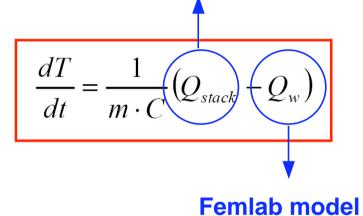
Maxwell – Stefan Eq.

Equations



Thermal model

The thermal dynamic behaviour of the FC system can be described by the following equation: $f(P_{el}, \eta)$



 Q_{stack} = generated heat flux

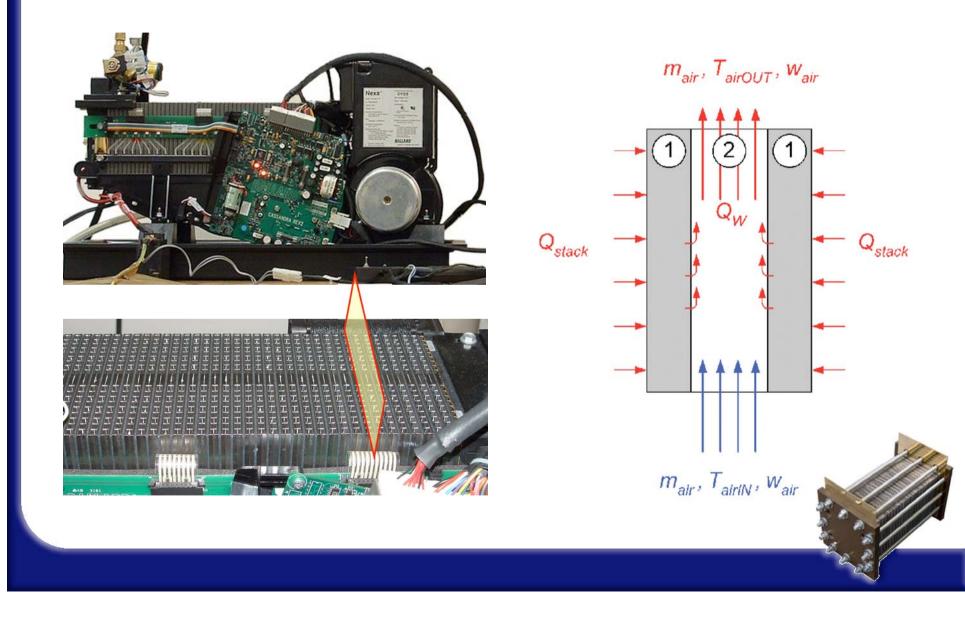
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Q_W = extracted heat flux
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Computational domain

The overall model was validated using the experimental data acquired on a **Ballard Nexa** 1.5 kWe PEM system



Thermal model - Computational domain

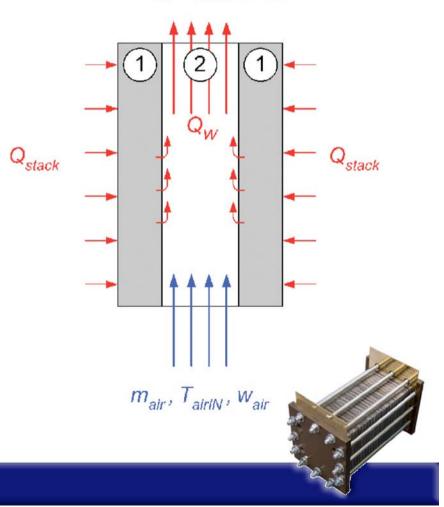


Thermal model - Equations

The thermal model is based on the Femlab Convection and Conduction application mode.

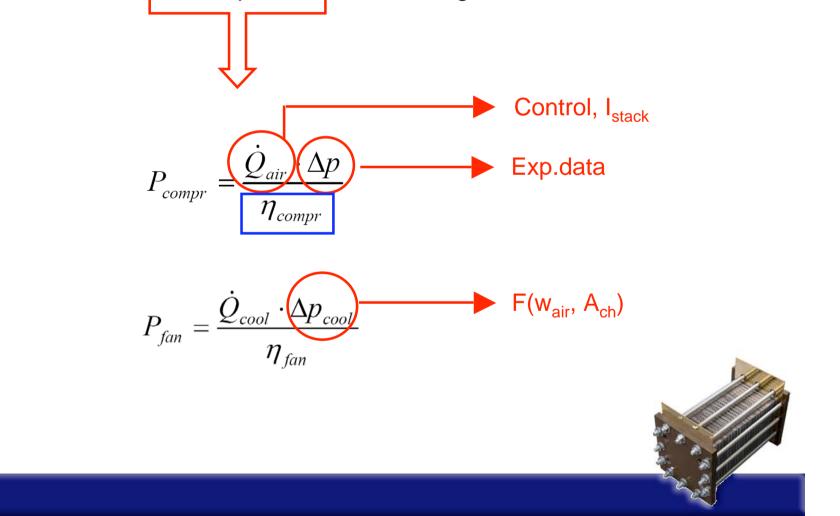
$$\nabla \cdot \left(-\,\alpha \nabla T + \rho C T \mathbf{u}\right) = Q$$





Auxiliaries model

Using simple models, it simulates the behavior of two main stack components: cathode air compressor and cooling fan.





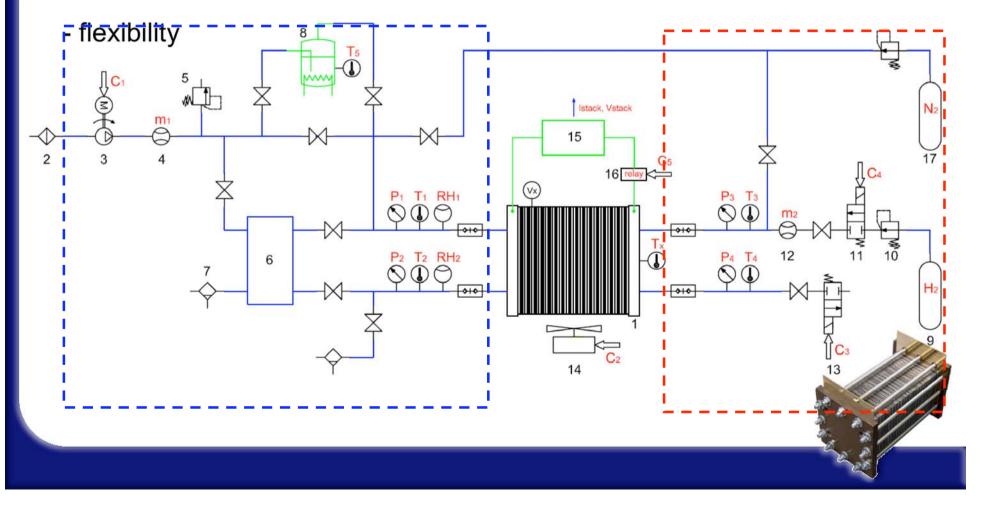
The preliminary experimentation phase was carried out using commercial hardware (Electrochem single cells and Ballard Nexa stack system) in order to set-up the experimental equipment, to understand the main issues regarding fuel cell operation and to validate the simulation model.

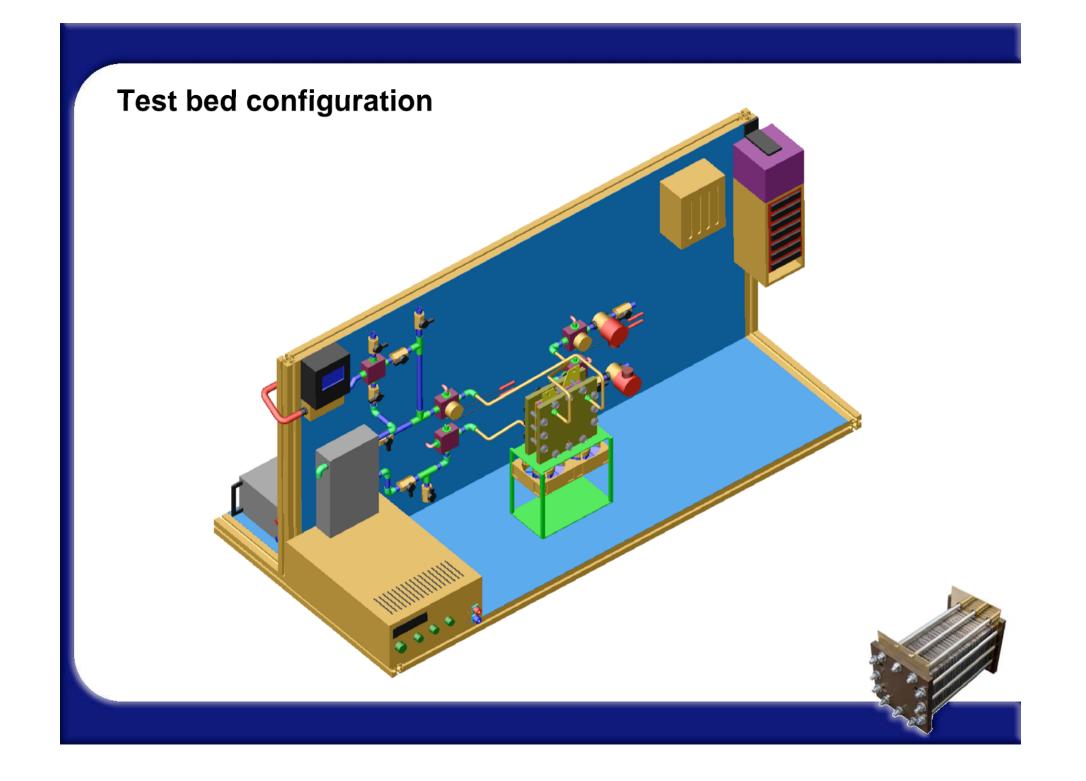


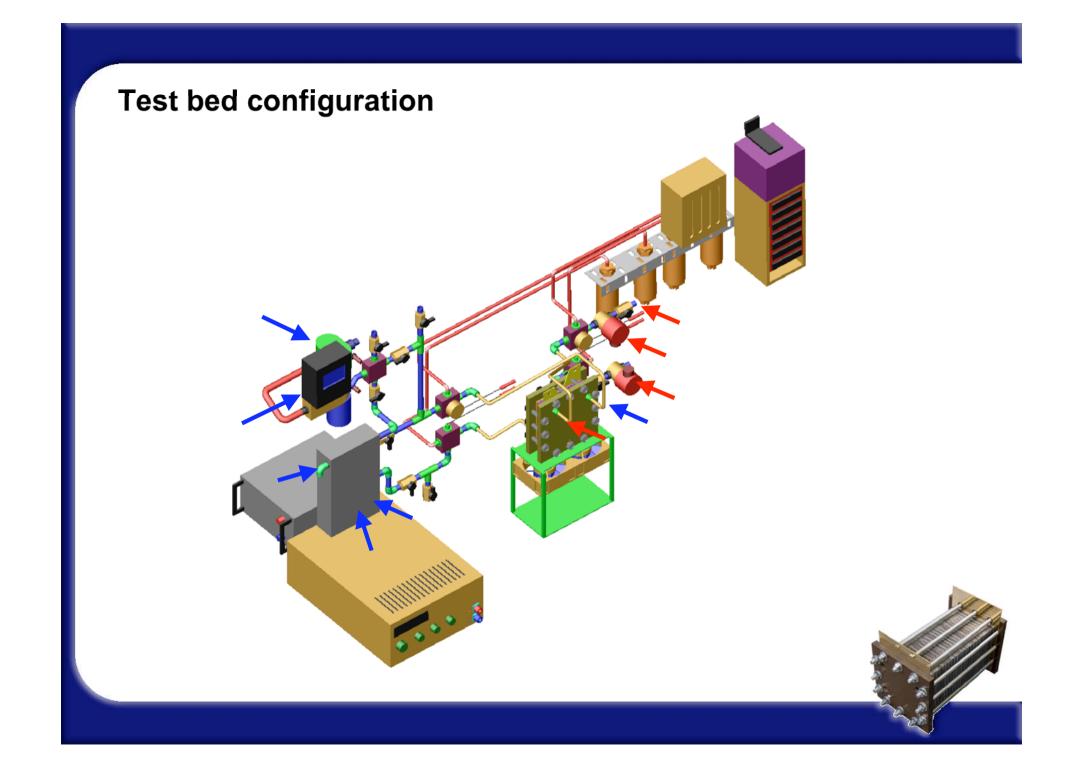
Test bed configuration

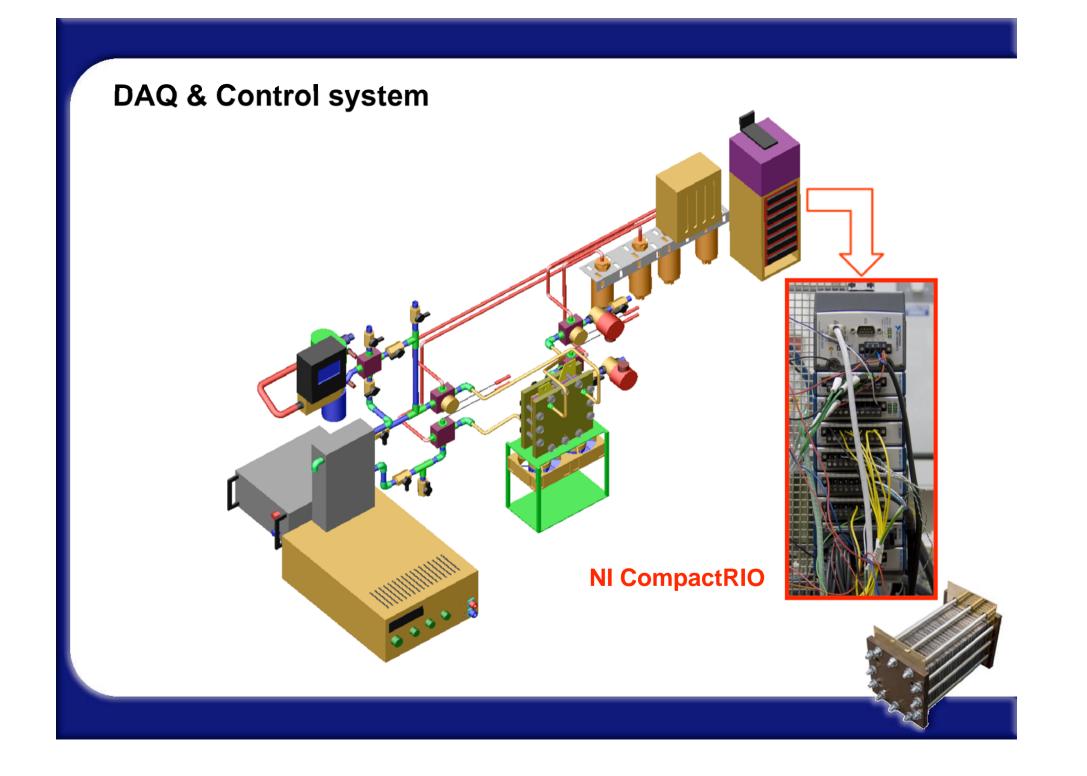
Requirements:

- DAQ of the fuel cell (stack) parameters
- control the fuel cell (stack) main functions

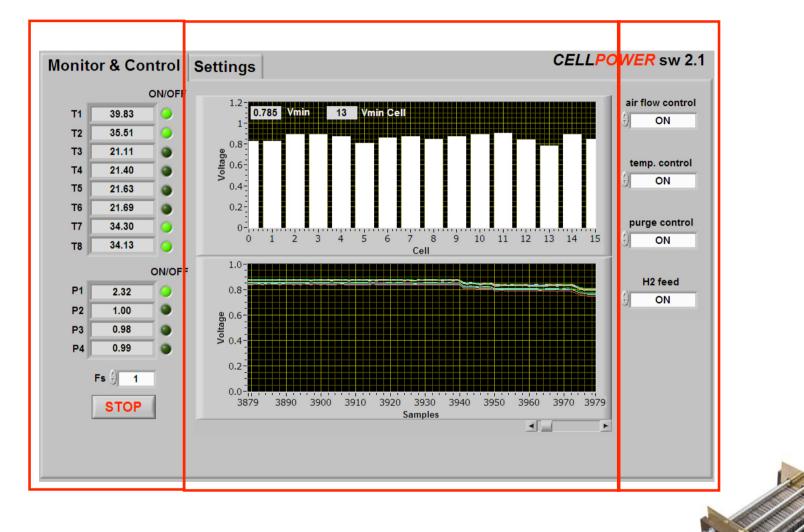








DAQ & Control software



Single cell tests

- hardware: Electrochem;
- experimental procedure: European project FCTESTNET, US Fuel Cell Council.

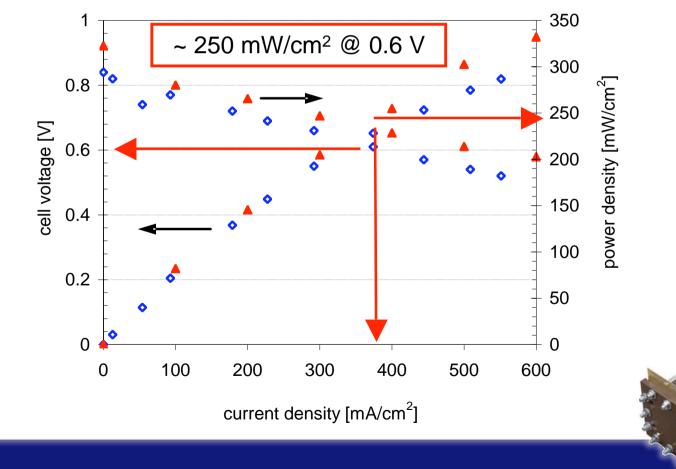


1 mg/cm ²	0.3 mg/cm ²
0	
1 mg/cm ²	0.6 mg/cm ²
Toray	SEAL tissue ⁸
Nafion 113	Nafion 113
Configuration #1	Configuration #2
	Nafion 113 Toray

CCM results

Polarization curve – Configuration #2

(air flow = 2.0 slpm, reactant gas pressure = 1.8 bar, cell temperature 45 °C, tightening torque 2.5 Nm). Red triangle marker – manufacturer data, blue rhomb marker – in house measured data.



Ballard Nexa tests

Targets:

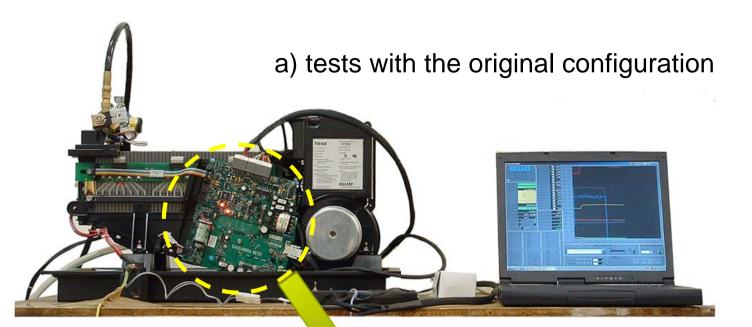
- understand the main issues regarding the stack operation
- test the monitoring and control system, implemented with the National Instruments platform



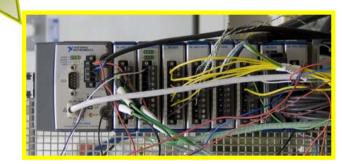
- 47 cells
- 1.5 kWe gross power
- 1.2 kWe nett power
- voltage = 43 V @ idle ÷ 26 V @ FL
- operates with pure hydrogen
- air cooled



Ballard Nexa tests

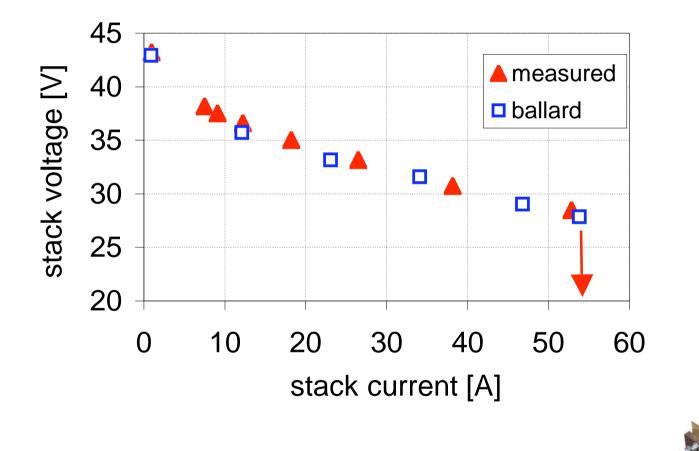


b) tests with the alternative controller



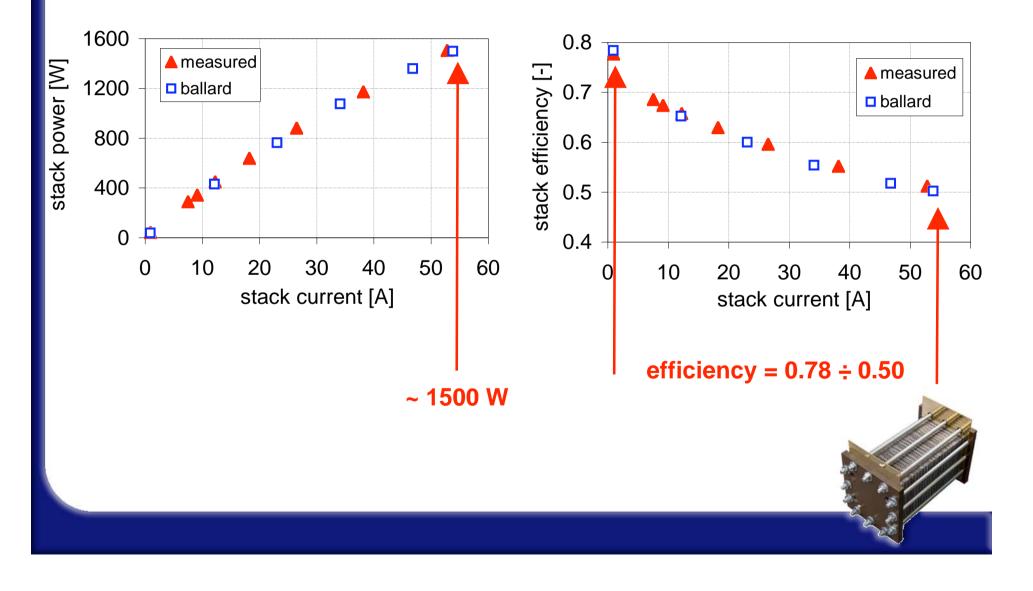
Ballard Nexa results – tests with the original configuration

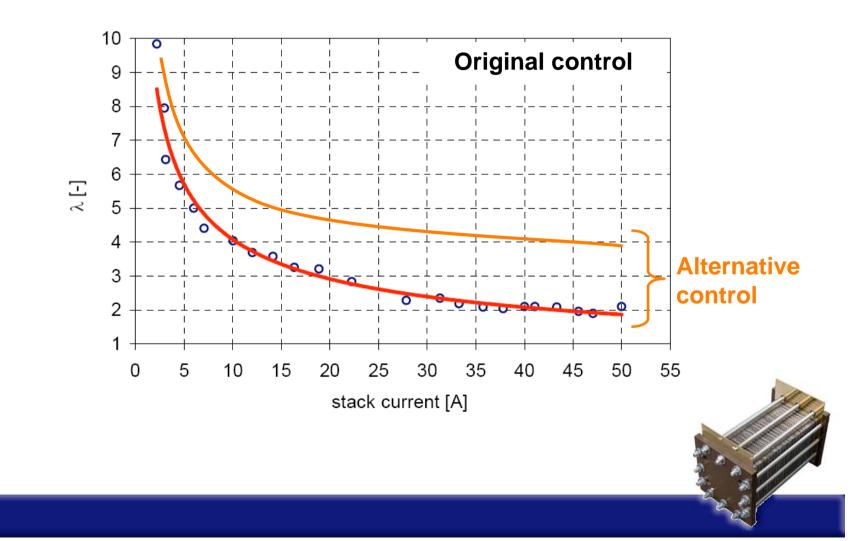
Comparison between measurements and manufacturer data

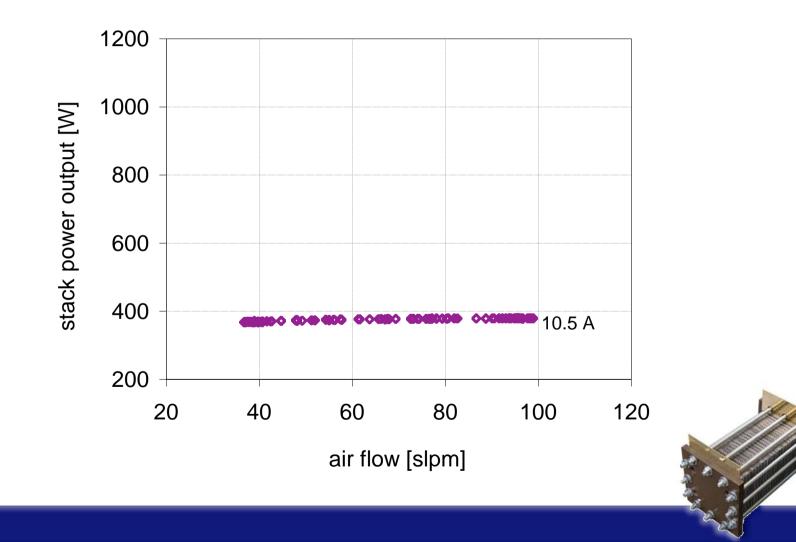


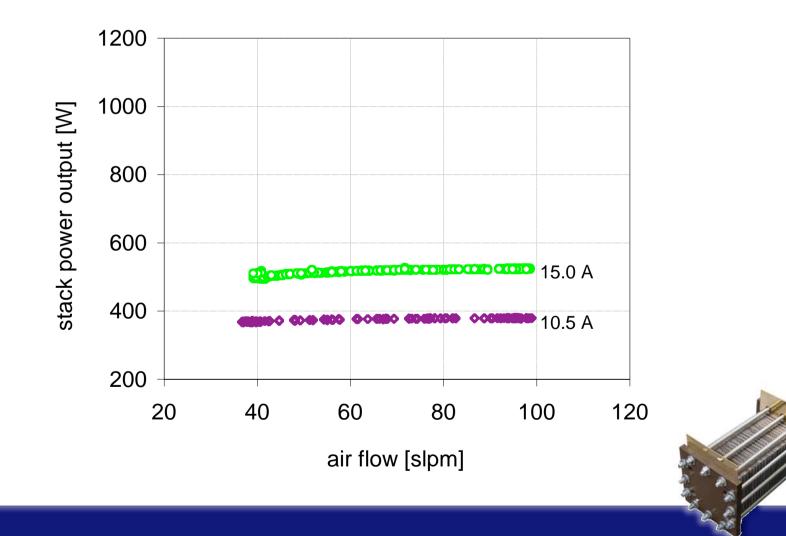
Ballard Nexa results – tests with the original configuration

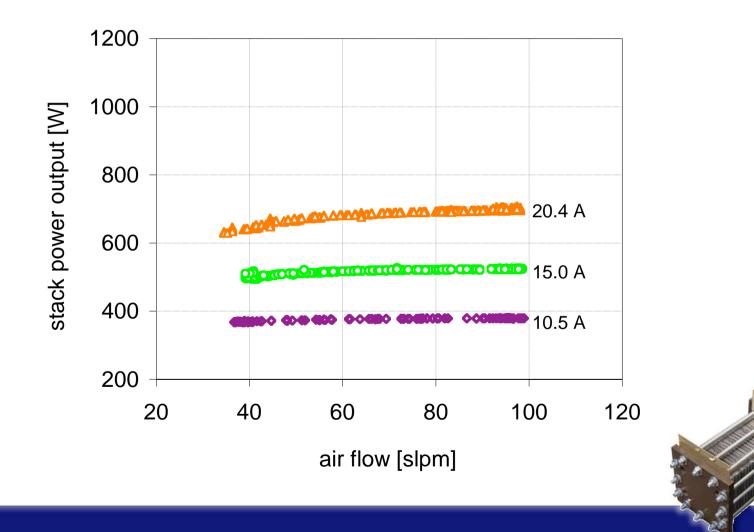
Comparison between measurements and manufacturer data

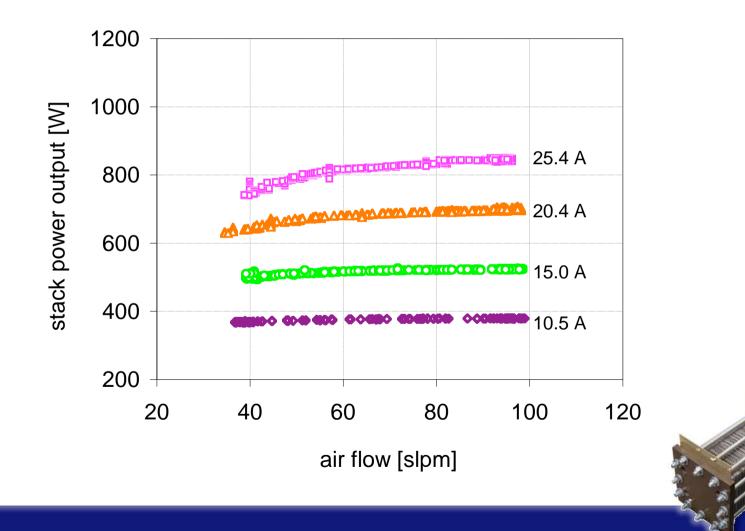


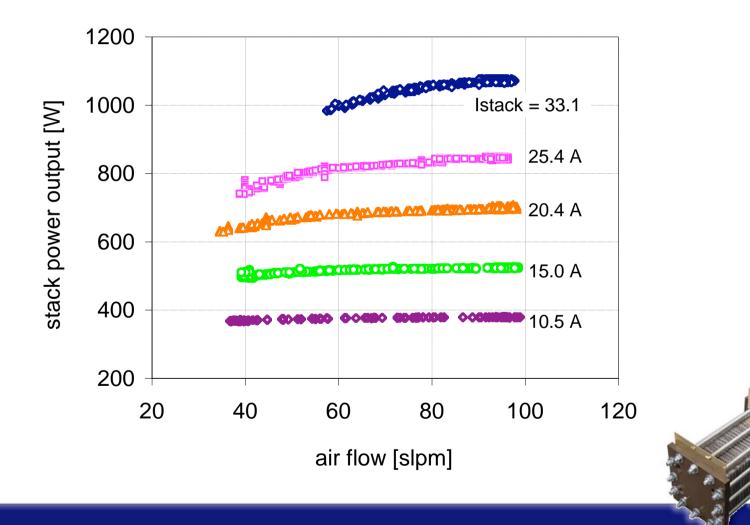




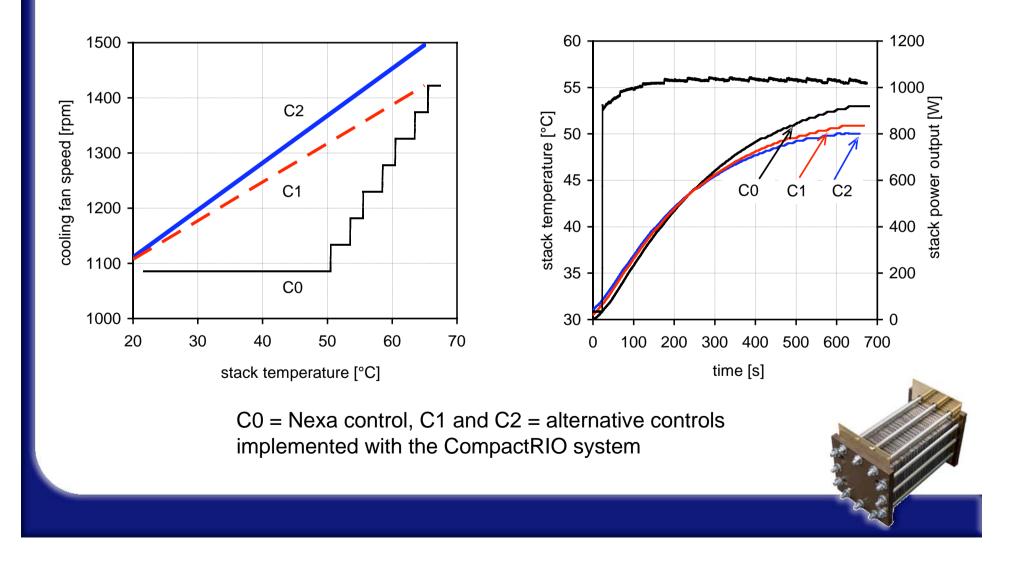






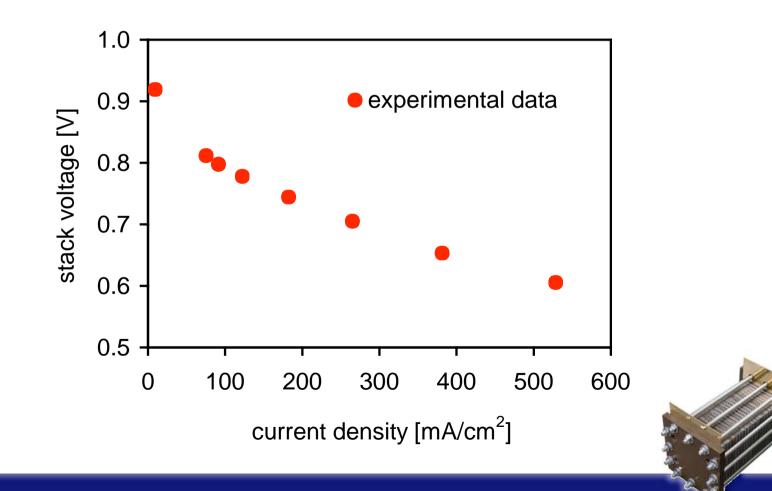


Temperature control



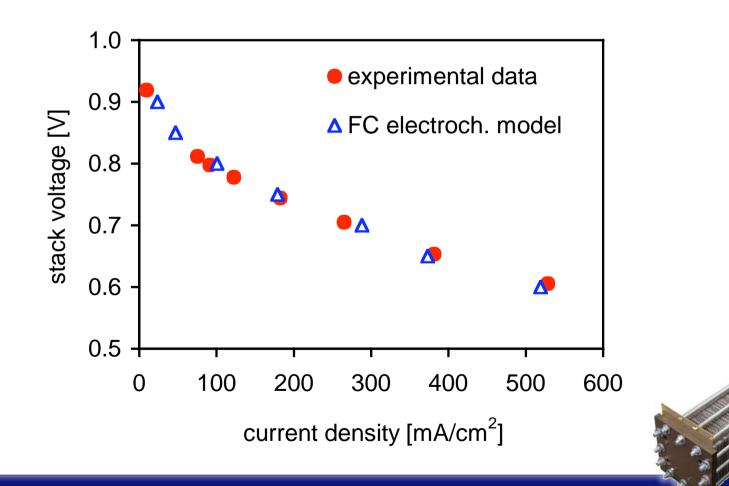
Ballard Nexa results – FC model validation

Electrochemical model



Ballard Nexa results – FC model validation

Electrochemical model

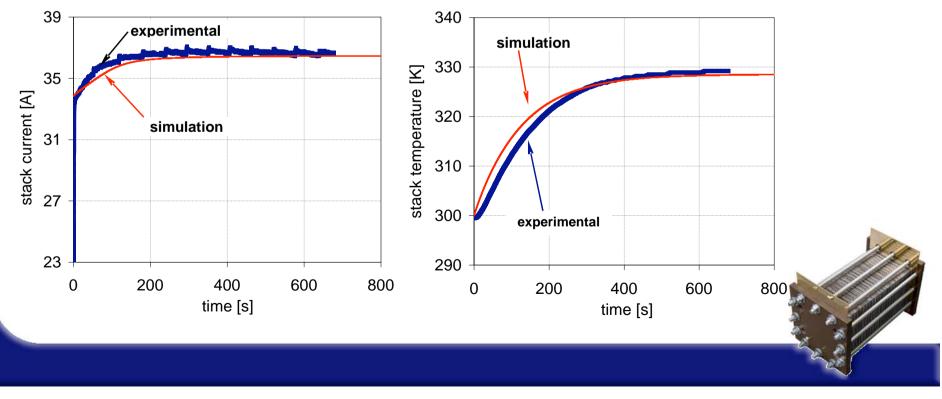


Ballard Nexa results – FC model validation

Thermal model

Stack power [W]	Measured Tstack [°C]	Calculated Tstack [°C]	Error [°C]	Error [%]
215	26.5	27.4	- 0.9	+ 3.3
1130	56.2	55.6	+ 0.6	- 1.1
1500	67.4	66.0	+ 1.4	- 2.1

Overall model





Stack design and testing

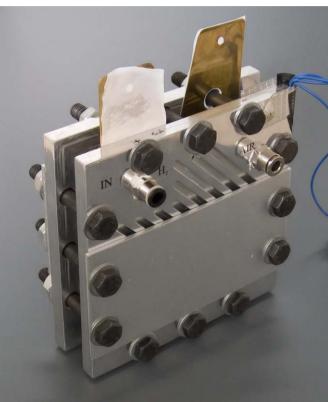
The development of the new system \rightarrow a two step approach:

• Stack#1 used to check if the chosen CCM offers the same performance on a stack system like on the single cell and to test the control system, especially on the temperature and purge controls.

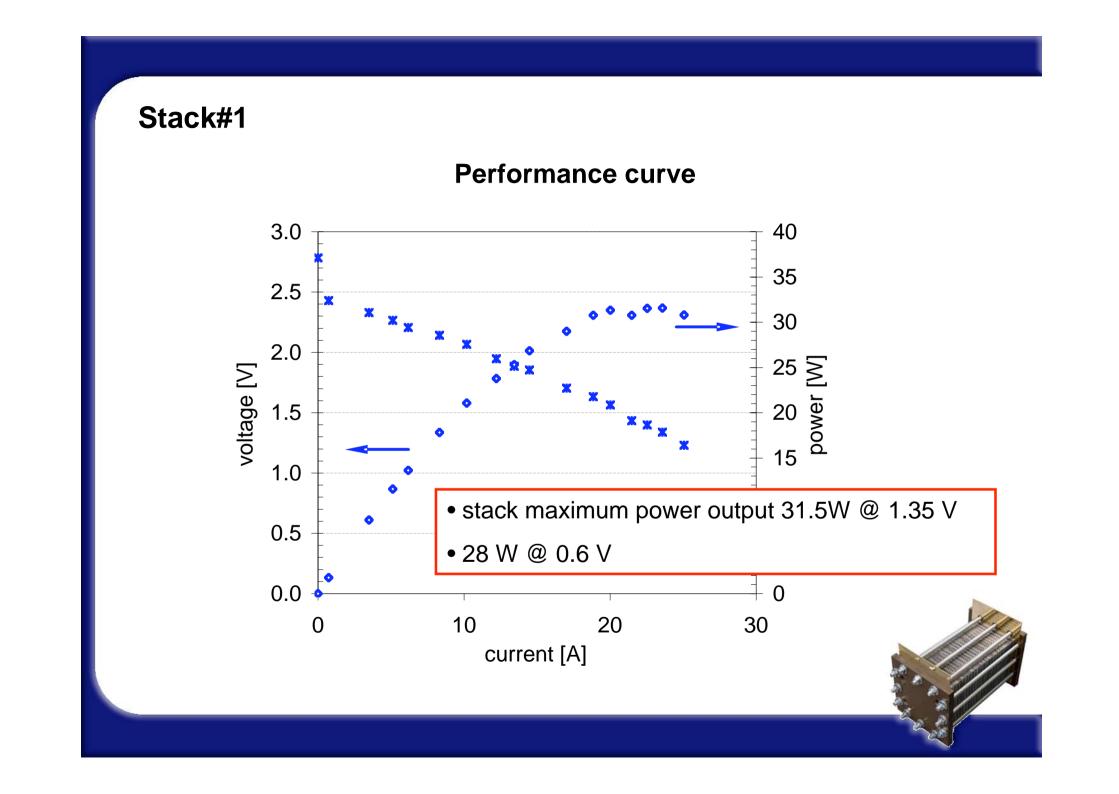
• Many issues that came up during the experimental activity on Stack#1 were useful for the designing of the final system, which will be called further Stack#2.

Stack#1

- three cell system
- 50 cm² CCM
- multiple serpentine BP
- serial feeding circuit
- dead end hydrogen circuit
- air cooling







Stack#1 **Control tests** Purge Temperature 0.65 0.60 stack temperature [°C] stack current [A] voltage [V] 0.55 0.50 0.45 0.40 time [s] time [s]



Stack#2 design and dimensioning

Number of cells

$$n_{cells} = \underbrace{\frac{P_{stack}}{A \cdot i \cdot V}}_{A \cdot i \cdot V} = 23 \ cells \longrightarrow 25 \ cells$$

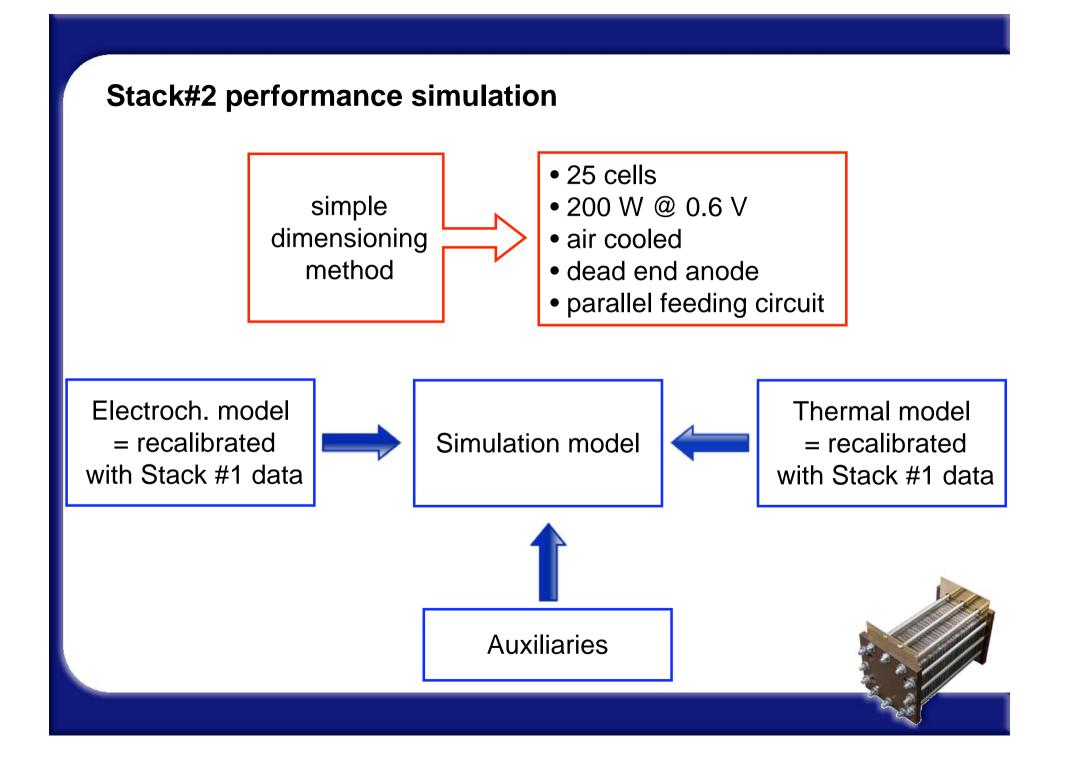
Stack voltage

$$V_{stack} = n_{cells} \cdot V = 15 V$$

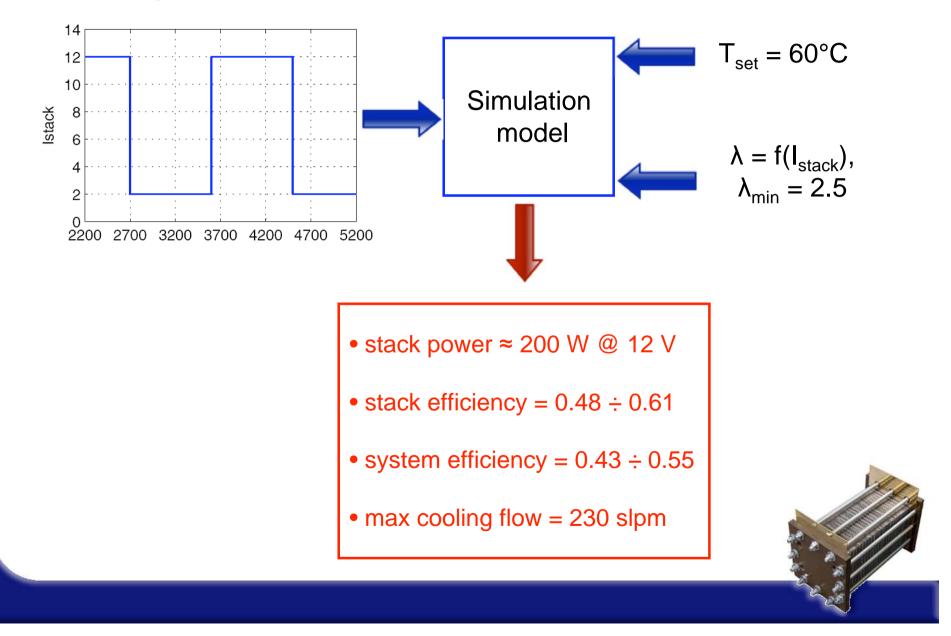
Stack current

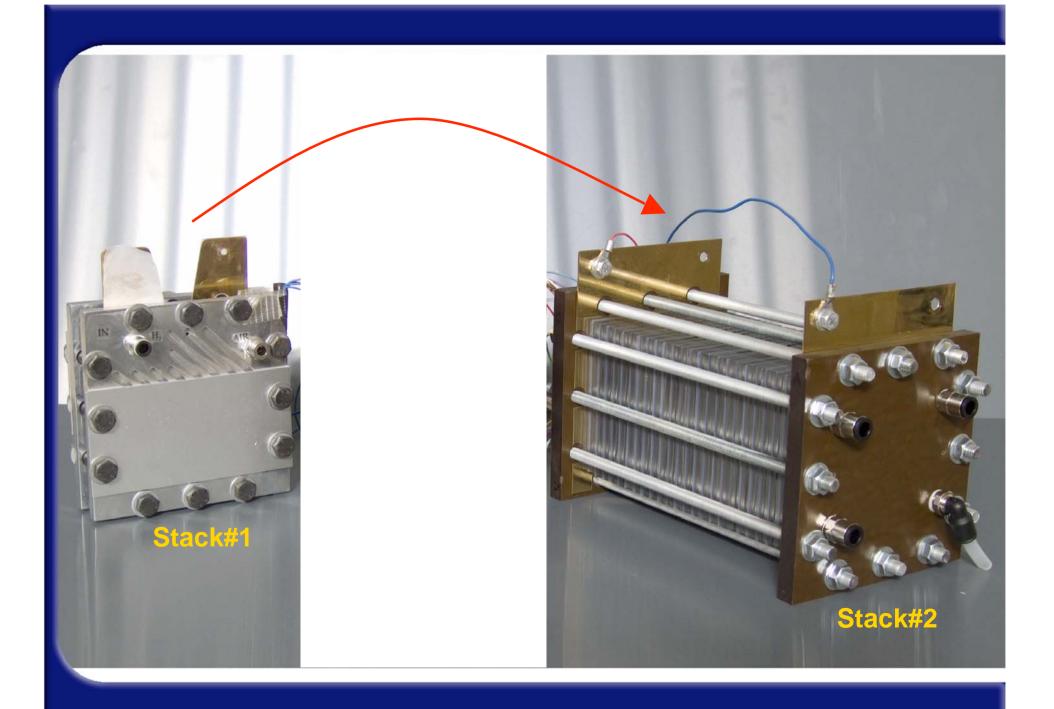
$$I_{stack} = i \cdot A = 15 A$$

Fuel cons.
$$\dot{m}_{fuel} = \frac{I_{stack} \cdot n_{cells}}{2 \cdot F} \cdot \frac{8.314 \cdot T_0}{p_0} \cdot 60 \cdot 10^3 = 2.9 \, slpm$$
Stoich. air. cons. $\dot{m}_{airST} = \frac{I_{stack} \cdot n_{cells}}{4 \cdot F} \cdot \frac{8.314 \cdot T_0}{p_0} \cdot 60 \cdot 10^3 = 6.9 \, slpm$ Air. cons. $\dot{m}_{air} \notin \lambda \cdot \dot{m}_{airST} = 17.3 \, slpm$ 2.5



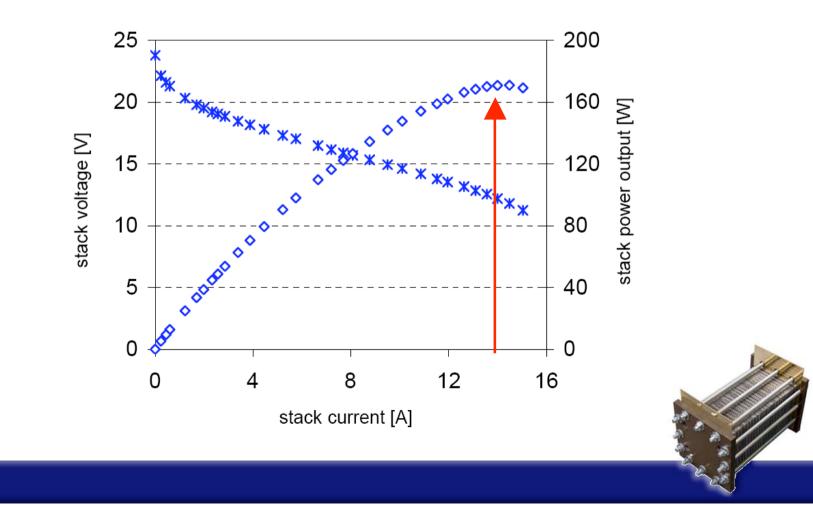
Stack#2 performance simulation





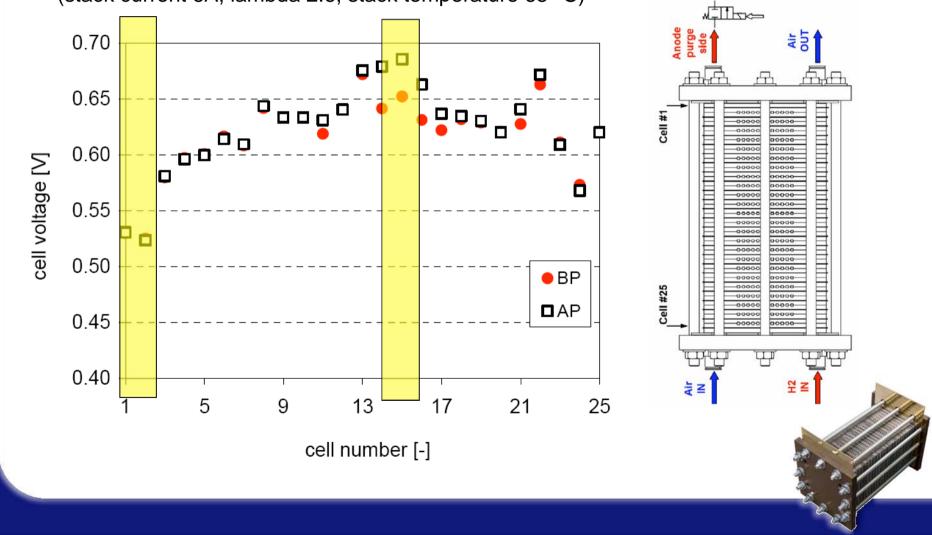
Stack#2 preliminary results

Stack#2 preliminary performance curves (after 21h conditioning, reactant gases pressure = 1.05 bar, stack temperature 60 °C)



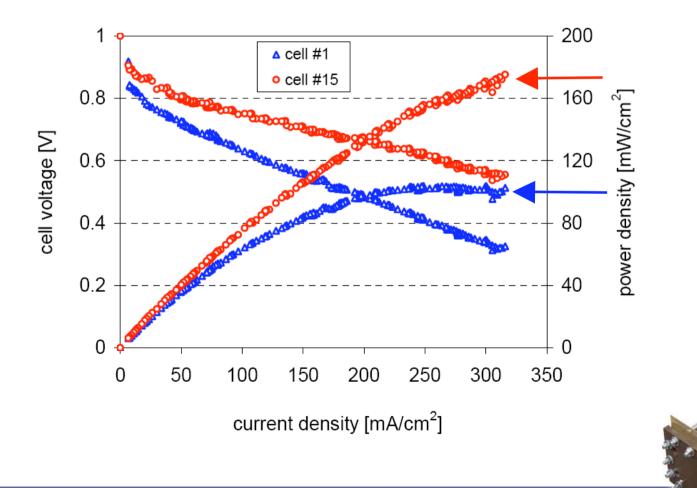
Stack#2 preliminary results

Voltage distribution before (BP) and after (AP) the anode purge (stack current 6A, lambda 2.6, stack temperature 65 °C)



Stack#2 preliminary results

Comparison between the best and worst performing cells



Final conclusions and future developments

- ✓ the simulation model proved its ability to simulate accurately the fuel cell
- \checkmark the potential of the data acquisition and control system was confirmed the
- ✓ accurate experimental procedure
- ✓ Stack#1 is able to reach a fair performance (31.5W @ 1.35 V)

✓ even if Stack#2 performance did not reach the expectations, it demonstrates that during the last three years, we succeed to build strong theoretical and experimental skills which will be applied on the development of further fuel cell based systems

✓ enhancement of the Stack#2 performance and to its integration in a self sustaining system

 \checkmark exploring other alternatives

